

Figure 3. Comparison of correlated and experimental solubilities.

such compounds one procedure is to calculate γ for the PNA of equal carbon number, then multiply this value by about 2.0, effectively halving the solubility. An alternative procedure is to follow the approach of Pierotti et al. (5) and calculate the activity coefficient of the parent (unsubstituted) hydrocarbon for alkyl-benzenes, then increase $\log \gamma$ by 0.622, i.e., a factor of 4.2 on γ , for each alkyl carbon present. The correlation obtained is shown in Figure 2 and has the form

$$\log \gamma_w^\infty = 3.5055 + 0.3417(N - 6) - 0.002640(N - 6)^2 \quad (4)$$

where N is carbon number. Correlated and experimental values of solubility excluding the alkyl substituted naphthalenes and

anthracenes are compared in Figure 3. The average deviation in log solubility is about 0.26 which corresponds to a factor of 1.8 but in some cases the deviation may be as high as a factor of 3. Although these deviations are large, the calculated solubilities are sufficiently accurate for many environmental calculation purposes. Since the correlation extends over 5 orders of magnitude and uses only carbon number and melting point, the accuracy is regarded as satisfactory. More accurate correlations will probably be developed when more thermal, solubility, and volumetric data are available for these compounds.

In conclusion, aqueous solubility data have been obtained for 32 PNA and indan. For approximate solubility estimation, the best procedure presently available for liquid hydrocarbons is to calculate γ_w^∞ from eq 4. The mole fraction solubility is then the reciprocal of γ_w^∞ . For solid hydrocarbons (i.e., melting point above 25 °C) γ^∞ can be calculated from eq 4, (f_s/f_l) from eq 3, and the solubility then calculated from eq 2. For alkyl-substituted naphthalenes or anthracenes the correlated solubilities are about double the experimental values and a correction of this magnitude is needed for such compounds.

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Vapor-Liquid Equilibrium of the Methane-*n*-Hexane System at Low Temperature

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Measurements of the bubble-point compositions are reported and combined with earlier dew-point data from this laboratory to give K values for the methane-*n*-hexane system at seven temperatures, 0, -25, -50, -63, -75, -80, and -82.65 °C, from 20 up to 2675 psia. The data may also be evaluated isobarically without interpolation. Two liquid phases were observed in the temperature region between -77.24 (UCST) and -90.69 °C (LCST); detailed composition measurements were made over this entire three-phase region and associated two-phase regions at a total of five temperatures. Equilibrium constants are reported for all three binaries encountered: G-L₁, G-L₂, and L₁-L₂.

A number of studies of the vapor-liquid equilibrium of the methane-*n*-hexane binary system have been reported in the literature. Both liquid and gas phases were studied by Boomer and Johnson (1) at 25, 55, and 85 °C and by Poston and McKetta (9) over the range 100-340 °F. The lowest temperatures were

studied by Shim and Kohn (11) in the range -110 to 150 °C, but they did not measure dew points below 0 °C or any bubble points near the critical pressure. Shim and Kohn did not report the two liquid phases existing at temperatures between -77.24 and -90.69 °C. Davenport and Rowlinson (7) reported, in a study of hydrocarbon solubilities in methane, that the methane-*n*-hexane system exhibited limited immiscibility, with an LCST of -90.6 °C. Earlier dew point studies in this laboratory (5) defined the three-phase region.

Experimental K values, obtained by combining the vapor-phase measurements of the elution method (5) with those obtained for the liquid phases by use of gas chromatography measurements, are presented here for the CH₄-*n*-C₆H₁₄ binary system. Equilibrium constants κ between the liquids for each component in this system are also evaluated.

Experimental Method and Procedure

The recycle equilibrium apparatus is the same as used by Elliot et al. (8) in the methane-*n*-butane investigation with some modifications. The boiling point of *n*-hexane is 68.95 °C.

Table I. Comparison of Dew Points Measured by the Elution and Chromatographic Methods

| Temp, °C (°F) | Pressure, psia | Pressure, kPa ^b | Methane mole fraction | |
|--------------------|-------------------|-------------------------------|-----------------------|-----------------------|
| | | | <i>y</i> | <i>y</i> ^a |
| 0.01 (32.02) | 20.1 | 138.58 | 0.9550 | 0.9558 |
| | 25.1 | 173.06 | 0.9623 | 0.9643 |
| | 50.1 | 345.43 | 0.9804 | 0.9815 |
| | 100.1 | 690.16 | 0.9872 | 0.9898 |
| | 150.1 | 1034.90 | 0.9916 | 0.9927 |
| -50.00 (-58.00) | 1600 | 11032 | 0.9890 | 0.9841 |

^a Experimental "elution" dew-point data from Chen et al. (5). ^b Pa: Pascal = kg/m s² = N/m²; 1 psia = 6.8947 kPa.

Therefore the problem of nonhomogeneous evaporation of the liquid phase in the sample line was more pronounced in this work than those encountered in the methane-*n*-butane (8) and methane-*n*-pentane systems (6). The temperature of the sampling lines was kept at more than 100 °C to transform and keep the sample in the vapor phase at essentially atmospheric conditions. A stirred pot with a volume of approximately 150 mL was used to homogenize the sample of the liquid phase (as a vapor) by mixing.

The experimental equipment and technique for the dew-point concentration data have been reported in detail in earlier publications (3-5) which should be consulted for itemized information.

In this bubble-point concentration investigation, a Barber-Coleman Gas Chromatograph Series 5000 Selecta System with flame ionization detection was used for analysis. The chromatographic column was a 4-ft length of 1/8 in. o.d. stainless steel tubing packed with 80-100 mesh Duopak (OPN/PORASIL C). Helium was used as a carrier gas. The flow rates of air and hydrogen were determined to give maximum response. Sample was introduced into the sample loop and then bubbled through a water column to indicate the flow rate of the sample. The signal from the detector was integrated by an Autolab Model 6300 digital integrator and recorded on a Leeds and Northrup strip chart recorder. Peak areas were calibrated by preparing gravimetric samples in sample bombs. The calibration was continually checked during the course of the entire study.

The pressure in the system was indicated by three (0-300, 0-1000, 0-4000 psia) Heise gages with accuracy 0.1% of the full scale reading.

Temperature was measured by a Leeds and Northrup certified platinum resistance thermometer and reported on the IPTS (1968) scale.

The experimental procedure was the same as used by Elliot. The isotherms were investigated in order of decreasing temperature and increasing pressure. In addition, after an isotherm was completed, additional points were sometimes verified on later dates to verify the consistency of the measurements and to fill the regions of uncertainty.

The bubble-point data were taken after completion of the dew-point investigation. Several experimental dew points were also measured here chromatographically to check the consistency of both experimental procedures. These points, which agreed within the combined accuracy of both experimental procedures, are tabulated in Table I.

An average of 3 h was required to attain steady state, after which at least six analyses were made.

Materials Used

Ultrahigh purity methane with a purity of 99.97 mol % minimum, manufactured by Union Carbide Chemicals Corp., was purchased from IWECO. Research grade *n*-hexane (99.99%)

was provided by Phillips Petroleum Co. and was used without further purification. A Model 451 A high-pressure purifier cartridge manufactured by Matheson Gas Products was used in the methane line to remove traces of oil, water, and particles down to approximately 12 μ.

Error Analysis

The error analysis is the same as Elliot's work because the same equipment and experimental procedure technique were used.

The contributing factors are temperature, controlled to 0.02 °C; pressure, measured by Heise gauges calibrated to 0.1% of full scale and controlled within 1 psi; and concentration, determined by chromatography from peak area ratios calibrated to a maximum error of 2% or 0.005 in mole fraction. The vast majority of the data are valid to four significant figures.

The overall error in the dew-point data is either less than 2% or 0.000 01 in mole fraction of *n*-hexane, depending on which is larger.

The maximum error in the resulting *K* values is 2%.

Results

Experimental results are shown in three tables.

Table I gives the dew points measured by both elution and chromatography methods for comparison purposes. The agreement is satisfactory.

Table II presents all experimental data except in the temperature-pressure region in which only two liquids exist without presence of vapor. The dew points and bubble points are shown along with limiting conditions. Equilibrium constants *K* are calculated for each component where data are available. Note that this table includes vapor-liquid equilibrium constants at the three-phase conditions. We define these by subscripts on the *K* to indicate the phases for which the *K* is calculated, with the third phase indicated outside parentheses. Thus, (*K*_{GL₂L₁}) indicates the vapor-liquid equilibrium constant between the gas *G* and liquid phase *L*₂ rich in heavy component (*n*-hexane) with light liquid *L*₁ rich in light component (methane) present.

The compositions of the two liquids in equilibrium with each other with no vapor present are shown in Table III. Equilibrium constants, *x*, defined as the ratio of concentrations of each component in the two liquids, are also reported in this table. Note that the first value at the lowest pressure in each isotherm is at the three-phase condition; hence these values are (*K*_{L₁L₂G}).

The pressure-composition behavior is given in Figure 1. Note that at -77.24 °C, which is the upper critical solution temperature (UCST), light liquid (*L*₁) is equal to vapor (*G*) at *p* = 755 psia. For *p* > 755 psia, light liquid (*L*₁') is in equilibrium with heavy liquid (*L*₂). At -90.69 °C, which is the lower critical solution temperature (LCST), light liquid (*L*₁') is equal to heavy liquid (*L*₂) at 495.3 psia. For *p* > 495.3 psia, light liquid (*L*₁) is in equilibrium with gas (*G*).

At any given temperature *τ* between the UCST and LCST, there exists a single fixed pressure *Π* at which all three phases are present at the same time. At *τ* for pressures greater than *Π* up to the respective criticals, only two phases are allowed: *L*₁-*G* or *L*₁'-*L*₂ depending on the total composition in the equilibrium cell.

In Figure 1, the dashed isobaric lines connect the three phase concentrations, which are equilibrium tie lines for that particular three-phase equilibrium. The dot-dash lines are the loci for *L*₂ and *L*₁ with vapor *G* present. This is a quantitative determination of the schematic Figure 1 lines *L*₁ and *L*₂ of ref 7. We must note, however, that we do not agree with the statement in the legend of Figure 1 (7) that "Seven of the curves shown in Fig. 3 are the projections of the liquid-phase boundary curves *L*₁PL₂." These values in Figure 3 of ref 7 must rather be *G*-*L*₂ equilibria at concentrations of methane less than the concentration of the LCST and be *G*-*L*₁ equilibria at concentrations of methane

Table II. Experimental Data of the Vapor-Liquid Equilibrium of the Methane-*n*-Hexane System

| <i>x</i> methane ^a | <i>y</i> methane ^b | psia | kPa ^c | <i>K</i> methane | <i>K n</i> -hexane |
|--|-------------------------------|-------------------|------------------|--------------------|--------------------|
| $T = 0.01\text{ }^{\circ}\text{C} = 32.02\text{ }^{\circ}\text{F} = 273.16\text{ K} = 427.65\text{ }^{\circ}\text{R}$ | | | | | |
| 0.0000 | 0.0000 | 0.83 ^d | 5.72 | 1120 ^e | 1.000 |
| 0.0097 | 0.9643 | 25.1 | 173.1 | 99.41 | 0.03605 |
| 0.0196 | 0.9815 | 50.1 | 345.4 | 50.08 | 0.1887 |
| 0.0387 | 0.9898 | 100.1 | 690.2 | 25.58 | 0.01061 |
| 0.0567 | 0.99266 | 150.1 | 1034.9 | 17.51 | 0.007781 |
| 0.0744 | 0.99396 | 200.1 | 1379.6 | 13.36 | 0.006525 |
| 0.1116 | 0.99528 | 300.1 | 2069.1 | 8.918 | 0.005313 |
| 0.1469 | 0.99566 | 400.1 | 2758.6 | 6.778 | 0.005087 |
| 0.2127 | 0.99578 | 600 | 4136.8 | 4.682 | 0.005360 |
| 0.2742 | 0.99549 | 800 | 5515.8 | 3.631 | 0.006214 |
| 0.3328 | 0.99465 | 1000 | 6894.7 | 2.989 | 0.008019 |
| 0.3886 | 0.99343 | 1200 | 8273.7 | 2.556 | 0.01075 |
| 0.4435 | 0.99166 | 1400 | 9652.6 | 2.236 | 0.01499 |
| 0.4924 | 0.9891 | 1600 | 11032 | 2.009 | 0.02147 |
| 0.5400 | 0.9849 | 1800 | 12410 | 1.824 | 0.03283 |
| 0.5933 | 0.9797 | 2000 | 13789 | 1.651 | 0.04991 |
| 0.6401 | 0.9692 | 2200 | 15168 | 1.514 | 0.08558 |
| 0.6564 | | 2300 | 15857 | | |
| 0.6949 | 0.9565 | 2400 | 16547 | 1.376 | 0.1426 |
| 0.7195 | | 2500 | 17237 | | |
| 0.7462 | 0.9400 ^f | 2550 | 17582 | 1.260 | 0.2364 |
| 0.7758 | 0.9366 | 2600 | 17926 | 1.207 | 0.2828 |
| 0.8025 | 0.9348 ^f | 2650 | 18271 | 1.165 | 0.3301 |
| 0.9290 | 0.9290 | 2675 ^h | 18443 | 1.000 | 1.000 |
| $T = -25.01\text{ }^{\circ}\text{C} = -13.02\text{ }^{\circ}\text{F} = 248.14\text{ K} = 446.65\text{ }^{\circ}\text{R}$ | | | | | |
| 0.000 | 0.0000 | 0.16 ^d | 1.1032 | 8800 ^e | 1.0000 |
| 0.009486 | 0.98990 | 20.1 | 138.58 | 104.4 | 0.01020 |
| 0.01152 | 0.99179 | 25.1 | 173.06 | 86.09 | 0.008306 |
| 0.02320 | 0.99557 | 50.1 | 345.43 | 42.91 | 0.004535 |
| 0.04638 | 0.99757 | 100.1 | 690.16 | 21.51 | 0.002548 |
| 0.06884 | 0.99817 | 150.1 | 1034.9 | 14.50 | 0.001965 |
| 0.08998 | 0.99847 | 200.1 | 1379.6 | 11.10 | 0.001681 |
| 0.1340 | 0.99872 | 300.1 | 2069.1 | 7.453 | 0.001478 |
| 0.1819 | 0.99879 | 400.1 | 2758.6 | 5.491 | 0.001479 |
| 0.2595 | 0.99863 | 600.1 | 4136.8 | 3.848 | 0.001850 |
| 0.3347 | 0.99820 | 800 | 5515.8 | 2.982 | 0.002706 |
| 0.3998 | 0.99759 | 1000 | 6894.7 | 2.495 | 0.004015 |
| 0.4672 | 0.99632 | 1200 | 8273.7 | 2.133 | 0.006907 |
| 0.5252 | 0.99416 | 1400 | 9652.6 | 1.893 | 0.01230 |
| 0.5804 | 0.99052 | 1600 | 11032 | 1.707 | 0.02259 |
| 0.6123 | 0.9889 ^f | 1700 | 11721 | 1.615 | 0.02863 |
| 0.6382 | 0.9844 | 1800 | 12410 | 1.542 | 0.04312 |
| 0.6937 | 0.9752 | 2000 | 13789 | 1.406 | 0.08097 |
| 0.7601 | 0.9644 | 2200 | 15168 | 1.269 | 0.1484 |
| 0.8191 | 0.9593 | 2300 | 15858 | 1.171 | 0.2250 |
| 0.9564 | 0.9564 | 2337 | 16113 | 1.000 | 1.000 |
| $T = -50.00\text{ }^{\circ}\text{C} = -58.00\text{ }^{\circ}\text{F} = 223.15\text{ K} = 401.67\text{ }^{\circ}\text{R}$ | | | | | |
| 0.0000 | 0.0000 | 0.25 ^d | 0.1724 | 32000 ^e | 1.000 |
| 0.01415 | 0.99841 | 20.2 | 139.27 | 70.56 | 0.001613 |
| 0.01710 | 0.99872 | 25.2 | 173.75 | 58.41 | 0.001302 |
| 0.03370 | 0.999343 | 50.2 | 346.12 | 29.65 | 0.0006799 |
| 0.06372 | 0.999632 | 100.2 | 690.85 | 15.69 | 0.0003930 |
| 0.09213 | 0.999713 | 150.2 | 1035.6 | 10.85 | 0.0003161 |
| 0.1218 | 0.999757 | 200.2 | 1380.3 | 8.211 | 0.0002767 |
| 0.1771 | 0.999775 | 300.2 | 2069.8 | 5.645 | 0.0002734 |
| 0.2294 | 0.999755 | 400.2 | 2759.3 | 4.358 | 0.0003179 |
| 0.3282 | 0.999594 | 600 | 4136.8 | 3.046 | 0.0006043 |
| 0.4207 | 0.999256 | 800 | 5515.8 | 2.375 | 0.001284 |
| 0.4952 | 0.99851 | 1000 | 6894.7 | 2.016 | 0.002952 |
| 0.5893 | 0.99613 | 1200 | 8273.7 | 1.690 | 0.009423 |
| 0.6518 | 0.99013 | 1400 | 9652.6 | 1.519 | 0.02835 |
| 0.7011 | 0.9871 | 1500 | 10342 | 1.408 | 0.04316 |
| 0.7423 | 0.9841 | 1600 | 11032 | 1.326 | 0.06170 |
| 0.7774 | 0.9816 | 1700 | 11721 | 1.263 | 0.08266 |
| 0.8022 | | 1750 | 12066 | | |
| 0.8189 | | 1775 | 12238 | | |
| 0.8444 | | 1790 | 12342 | | |
| 0.8522 | | 1800 | 12410 | | |
| 0.8922 | | 1803 | 12431 | | |
| 0.9784 | 0.9784 | 1804 ^h | 12438 | 1.000 | 1.000 |

Table II (continued)

| x methane ^a | y methane ^b | psia | kPa ^c | K methane | K n-hexane |
|---|------------------------|----------------------|------------------|---------------------|------------|
| $T = -63.00\text{ }^{\circ}\text{C} = -81.40\text{ }^{\circ}\text{F} = 210.15\text{ K} = 378.27\text{ }^{\circ}\text{R}$ | | | | | |
| 0.0000 | 0.0000 | 0.008 ^d | 0.0552 | 76000 ^e | 1.000 |
| 0.01583 | 0.999495 | 20.2 | 139.27 | 63.95 | 0.0005130 |
| 0.01867 | 0.999589 | 25.2 | 173.75 | 53.54 | 0.0004188 |
| 0.03782 | 0.999781 | 50.2 | 346.12 | 26.44 | 0.0002276 |
| 0.07307 | 0.999868 | 100.2 | 690.85 | 13.68 | 0.0001424 |
| 0.1079 | 0.999888 | 150.2 | 1035.6 | 9.264 | 0.0001256 |
| 0.1411 | 0.999903 | 200.2 | 1380.3 | 7.087 | 0.0001129 |
| 0.2071 | 0.999894 | 300.2 | 2069.8 | 4.828 | 0.0001337 |
| 0.2700 | 0.999878 | 400.2 | 2759.3 | 3.703 | 0.0001671 |
| 0.3881 | 0.999798 | 600 | 4136.8 | 2.576 | 0.0003301 |
| 0.5139 | 0.999402 | 800 | 5515.8 | 1.945 | 0.001230 |
| 0.6162 | 0.99730 | 1000 | 6894.7 | 1.618 | 0.007036 |
| 0.7156 | 0.99177 | 1200 | 8273.7 | 1.386 | 0.02894 |
| 0.7576 | | 1300 | 8963.1 | | |
| 0.8091 | 0.9882 | 1400 | 9652.6 | 1.221 | 0.06181 |
| 0.8279 | | 1420 | 9790.5 | | |
| 0.8568 | | 1435 | 9893.9 | | |
| 0.8713 | | 1440 | 9928.4 | | |
| 0.9872 | 0.9872 | 1443 ^h | 9949.1 | 1.000 | 1.000 |
| $T = -75.10\text{ }^{\circ}\text{C} = -103.18\text{ }^{\circ}\text{F} = 198.05\text{ K} = 356.49\text{ }^{\circ}\text{R}$ | | | | | |
| 0.0000 | 0.0000 | 0.002 ^d | 0.0138 | 200000 ^e | 1.000 |
| 0.01950 | 0.999848 | 19.9 | 137.21 | 51.28 | 0.000155 |
| 0.02438 | 0.999885 | 25.0 | 172.37 | 41.02 | 0.000118 |
| 0.04742 | 0.999927 | 50.0 | 344.74 | 21.09 | 0.0000766 |
| 0.09603 | 0.999949 | 100.0 | 689.47 | 10.41 | 0.0000564 |
| 0.1390 | 0.999955 | 150.0 | 1034.2 | 7.194 | 0.0000523 |
| 0.1813 | 0.999952 | 200.0 | 1378.9 | 5.515 | 0.0000586 |
| 0.2660 | 0.999939 | 300.0 | 2068.4 | 3.760 | 0.0000831 |
| 0.3412 | 0.999919 | 400.0 | 2757.9 | 2.931 | 0.000123 |
| 0.4225 | 0.999893 | 500.0 | 3447.4 | 2.367 | 0.000185 |
| 0.5076 | 0.999832 | 600.0 | 4136.8 | 1.970 | 0.000341 |
| 0.5936 | 0.999640 | 700 | 4826.3 | 1.684 | 0.000886 |
| 0.6872 | 0.99789 | 800 | 5515.8 | 1.452 | 0.00675 |
| 0.7596 | 0.99572 | 900 | 6205.3 | 1.311 | 0.0178 |
| 0.8117 | 0.99435 | 1000 | 6894.7 | 1.225 | 0.0300 |
| 0.8468 | | 1050 | 7239.5 | | |
| 0.8932 | | 1055 | 7273.9 | | |
| 0.99364 | 0.99364 | 1057 ^h | 7287.7 | 1.000 | 1.000 |
| $T = -77.24\text{ }^{\circ}\text{C} = -107.03\text{ }^{\circ}\text{F} = 195.91\text{ K} = 352.64\text{ }^{\circ}\text{R}$ | | | | | |
| 0.0000 | | 0.007 ^d | 0.048 | | |
| 0.02082 | | 20.0 | 137.89 | | |
| 0.04831 | | 50.0 | 344.74 | | |
| 0.09528 | | 100 | 689.47 | | |
| 0.1407 | | 150 | 1034.2 | | |
| 0.1849 | | 200 | 1378.9 | | |
| 0.2698 | | 300 | 2068.4 | | |
| 0.3555 | | 400 | 2757.9 | | |
| 0.4429 | | 500 | 3447.4 | | |
| 0.5323 | | 600 | 4136.8 | | |
| 0.6422 | | 700 | 4826.3 | | |
| 0.7177 | 0.99763 | 755 ⁱ | 5205.5 | 1.390 | 0.00840 |
| $T = -80.00\text{ }^{\circ}\text{C} = -112.00\text{ }^{\circ}\text{F} = 193.15\text{ K} = 347.60\text{ }^{\circ}\text{R}$ | | | | | |
| 0.0000 | 0.0000 | 0.0013 ^d | 0.00896 | 280000 ^e | 1.000 |
| 0.02210 | 0.999905 | 20.1 | 138.58 | 45.25 | 0.0000972 |
| 0.02728 | 0.999932 | 25.1 | 173.06 | 36.65 | 0.0000699 |
| 0.09964 | 0.999964 | 100.1 | 690.16 | 10.04 | 0.0000400 |
| 0.2851 | 0.999970 | 300.1 | 2069.1 | 3.508 | 0.0000420 |
| 0.4697 | 0.999932 | 500.1 | 3447.4 | 2.129 | 0.000128 |
| 0.5802 | 0.999830 | 600 | 4136.8 | 1.723 | 0.000405 |
| 0.6902 | 0.999567 | 675 | 4653.9 | 1.448 | 0.00140 |
| 0.7239 | 0.999393 | 692 ⁱ | 4771.2 | 1.381 | 0.00220 |
| 0.9864 (L ₁) | 0.999393 | 692 ⁱ | 4771.2 | 1.013 | 0.0446 |
| 0.9914 (L ₁) | 0.99898 | 700 | 4826.3 | 1.008 | 0.119 |
| 0.9988 (L ₁) | 0.99882 | 708 ⁱ | 4881.5 | 1.000 | 1.000 |
| $T = -82.65\text{ }^{\circ}\text{C} = -116.77\text{ }^{\circ}\text{F} = 190.50\text{ K} = 342.90\text{ }^{\circ}\text{R}$ | | | | | |
| 0.0000 | 0.0000 | 0.00093 ^d | 0.00641 | 350000 ^e | 1.000 |
| 0.02256 | 0.999924 | 20.0 | 137.89 | 44.33 | 0.0000778 |
| 0.02803 | 0.999960 | 25.0 | 172.37 | 35.68 | 0.0000412 |
| 0.1047 | 0.999970 | 100.0 | 689.47 | 9.548 | 0.0000335 |

Table II (continued)

| x methane ^a | y methane ^b | psia | kPa ^c | K methane | K n-hexane |
|---|------------------------|----------------------|------------------|-----------|------------|
| 0.3004 | 0.999988 | 300.0 | 2068.4 | 3.329 | 0.0000172 |
| 0.5041 | 0.999907 | 499.6 | 3444.6 | 1.984 | 0.000188 |
| 0.6487 | 0.999814 | 600 | 4136.8 | 1.541 | 0.000529 |
| 0.7438 | 0.999611 | 638 ⁱ | 4398.8 | 1.344 | 0.00152 |
| 0.9695 (L ₁) | 0.999611 | 638 ⁱ | 4398.8 | 1.031 | 0.0128 |
| 0.9724 (L ₁) | 0.999577 | 645 ⁱ | 4447.1 | 1.028 | 0.0153 |
| 0.9745 (L ₁) | 0.999587 | 650 | 4481.6 | 1.026 | 0.0162 |
| 0.9897 (L ₁) | 0.999609 | 655 | 4516.1 | 1.010 | 0.0380 |
| 0.9919 (L ₁) | 0.999687 | 660 | 4550.5 | 1.008 | 0.0386 |
| 0.999847 (L ₁) | 0.99847 | 665 ^h | 4565.0 | 1.000 | 1.000 |
| T = -86.92 °C = -124.46 °F = 186.23 K = 335.21 °R | | | | | |
| 0.0000 | | 0.00054 ^d | 0.00372 | | |
| 0.06129 | | 50.0 | 344.74 | | |
| 0.1189 | | 100 | 689.47 | | |
| 0.1813 | | 150 | 1034.2 | | |
| 0.2357 | | 200 | 1378.9 | | |
| 0.3412 | | 300 | 2068.4 | | |
| 0.4593 | | 400 | 2757.9 | | |
| 0.6010 | | 500 | 3447.4 | | |
| 0.6826 | | 540 | 3723.2 | | |
| 0.8057 | 0.999837 | 559 ⁱ | 3854.1 | 1.241 | 0.000839 |
| 0.9505 (L ₁) | 0.999837 | 559 ⁱ | 3854.1 | 1.052 | 0.00329 |
| 0.9776 (L ₁) | | 574 | 3957.6 | | |
| 0.9871 (L ₁) | | 579 | 3992.0 | | |
| 1.000 (L ₁) | | 582 ^g | 4012.7 | | |
| T = -90.69 °C = -131.24 °F = 182.46 K = 328.43 °R | | | | | |
| (LCST) | | | | | |
| 0.0000 | | 0.00034 ^d | 0.00234 | | |
| 0.02766 | | 20.0 | 137.89 | | |
| 0.03463 | | 25.0 | 172.37 | | |
| 0.06623 | | 50.0 | 344.74 | | |
| 0.1308 | | 100 | 689.47 | | |
| 0.1907 | | 150 | 1034.2 | | |
| 0.2560 | | 200 | 1378.9 | | |
| 0.3822 | | 300 | 2068.4 | | |
| 0.5178 | | 400 | 2757.9 | | |
| 0.6100 | | 450 | 3102.6 | | |
| 0.7426 | | 480 | 3309.5 | | |
| 0.9286 | 0.999946 | 495.3 ⁱ | 3414.9 | 1.077 | 0.000756 |
| 0.9640 (L ₁) | | 510 | 3516.3 | | |
| 0.9876 (L ₁) | | 515 | 3550.8 | | |
| 1.000 (L ₁) | | 516 ^g | 3557.7 | | |

^a All liquid-phase data are L₂ unless otherwise noted. ^b Vapor compositions from Chen et al. (5), except as noted by f. ^c Pa: Pascal = kg/m s² = N/m²; 1 psia = 6.8947 kPa. ^d Vapor pressure of n-hexane from Carruth (2). ^e K_{CH₄}. ^f Dew points measured by chromatography. ^g Vapor pressure of CH₄. ^h Critical pressure where liquid ≡ gas. ⁱ Pressure at which L₁-L₂-G exists.

Table III. Liquid-Liquid Equilibrium Data of the Methane-n-Hexane System^a

| x methane (L ₂) | x' methane (L ₁ ') ^b | psia | kPa | κ methane | κ n-hexane |
|---|--|------------------|--------|-----------|------------|
| T = -77.24 °C = -107.03 °F = 195.91 K = 352.64 °R | | | | | |
| (UCST L ₁ ≡ G) | | | | | |
| 0.7177 | 0.9976 | 755 ^c | 5205.5 | 1.3900 | 0.008502 |
| 0.7425 | 0.9851 | 800 | 5515.8 | 1.3267 | 0.05786 |
| 0.7701 | 0.9769 | 850 | 5860.5 | 1.2685 | 0.1005 |
| 0.7809 | 0.9674 | 880 | 6067.4 | 1.2388 | 0.1488 |
| 0.7950 | 0.9520 | 910 | 6274.2 | 1.1975 | 0.2342 |
| 0.8151 | 0.9390 | 950 | 6550.0 | 1.1520 | 0.3840 |
| 0.8416 | 0.9133 | 975 | 6722.4 | 1.0852 | 0.5474 |
| 0.8900 ^b | 0.8900 ^b | 986 ^d | 6798.2 | 1.000 | 1.000 |
| T = -80.00 °C = -112.00 °F = 193.15 K = 347.67 °R | | | | | |
| 0.7239 | 0.9864 | 692 ^c | 4771.2 | 1.3626 | 0.04926 |
| 0.7415 | 0.9785 | 720 | 4964.2 | 1.3196 | 0.08317 |
| 0.7531 | 0.9716 | 740 | 5102.1 | 1.2901 | 0.1150 |
| 0.7649 | 0.9660 | 760 | 5240.0 | 1.2629 | 0.1446 |
| 0.7858 | 0.9522 | 800 | 5515.8 | 1.2118 | 0.2232 |
| 0.7949 | 0.9445 | 820 | 5635.7 | 1.1882 | 0.2706 |
| 0.8098 | 0.9377 | 840 | 5791.6 | 1.1579 | 0.3276 |

Table III. (continued)

| x methane (L ₂) | x' methane (L ₁ ') | psia | kPa | κ methane | κ n-hexane |
|---|-------------------------------|--------------------|--------|-----------|------------|
| 0.8278 | 0.9238 | 860 | 5929.5 | 1.1160 | 0.4425 |
| 0.9004 | 0.9004 | 883 ^d | 6088.1 | 1.000 | 1.000 |
| $T = -82.65\text{ }^{\circ}\text{C} = -116.77\text{ }^{\circ}\text{F} = 190.50\text{ K} = 342.90\text{ }^{\circ}\text{R}$ | | | | | |
| 0.7438 | 0.9695 | 638 ^c | 4398.8 | 1.3034 | 0.1191 |
| 0.7756 | 0.9631 | 675 | 4653.9 | 1.2418 | 0.1644 |
| 0.7829 | 0.9486 | 700 | 4826.3 | 1.2117 | 0.2368 |
| 0.8042 | 0.9369 | 725 | 4998.7 | 1.1650 | 0.3223 |
| 0.8071 | 0.9484 | 730 | 5033.1 | 1.1751 | 0.2675 |
| 0.8297 | 0.9280 | 760 | 5240.0 | 1.1185 | 0.4228 |
| 0.8975 | 0.8975 | 770 ^d | 5308.9 | 1.000 | 1.000 |
| $T = -86.92\text{ }^{\circ}\text{C} = -124.46\text{ }^{\circ}\text{F} = 186.23\text{ K} = 335.21\text{ }^{\circ}\text{R}$ | | | | | |
| 0.8057 | 0.9505 | 559 ^c | 3854.2 | 1.1797 | 0.2548 |
| 0.8199 | 0.9412 | 580 | 3998.9 | 1.1479 | 0.3265 |
| 0.8313 | 0.9335 | 600 | 4136.8 | 1.1229 | 0.3942 |
| 0.8515 | 0.9246 | 612 | 4219.6 | 1.0858 | 0.5077 |
| 0.9013 | 0.9013 | 624 | 4302.3 | 1.000 | 1.000 |
| $T = -90.69\text{ }^{\circ}\text{C} = -131.24\text{ }^{\circ}\text{F} = 182.46\text{ K} = 328.43\text{ }^{\circ}\text{R}$ | | | | | |
| (LCST L ₁ ' ≡ L ₂) | | | | | |
| 0.9286 | 0.9286 | 495.3 ^c | 3414.9 | 1.000 | 1.000 |

^a Except at pressure indicated with footnote c, no gas phase is present. ^b Estimated value. ^c L₁-L₂-G. ^d L₁ ≡ L₂.

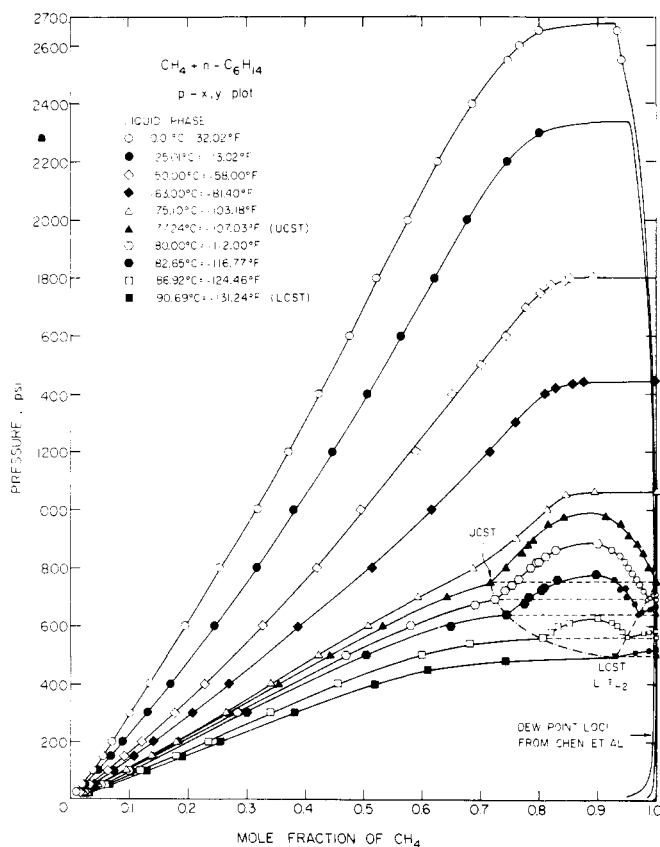


Figure 1. Pressure-composition diagram for the methane-n-hexane system.

greater than the LCST. Nevertheless, the technique of Davenport and Rowlinson (7) does yield a value for the LCST quite close to our value: 182.6 K and 0.30 weight fraction n-hexane (0.926 mole fraction methane) as compared to our -90.69 °C (182.46 K) and 0.9286 mole fraction methane.

Note also that for the isotherm at -75 °C, which is slightly more than 2 °C above the UCST, the shape of the p-x plot is affected.

K values for each temperature as a function of pressure are

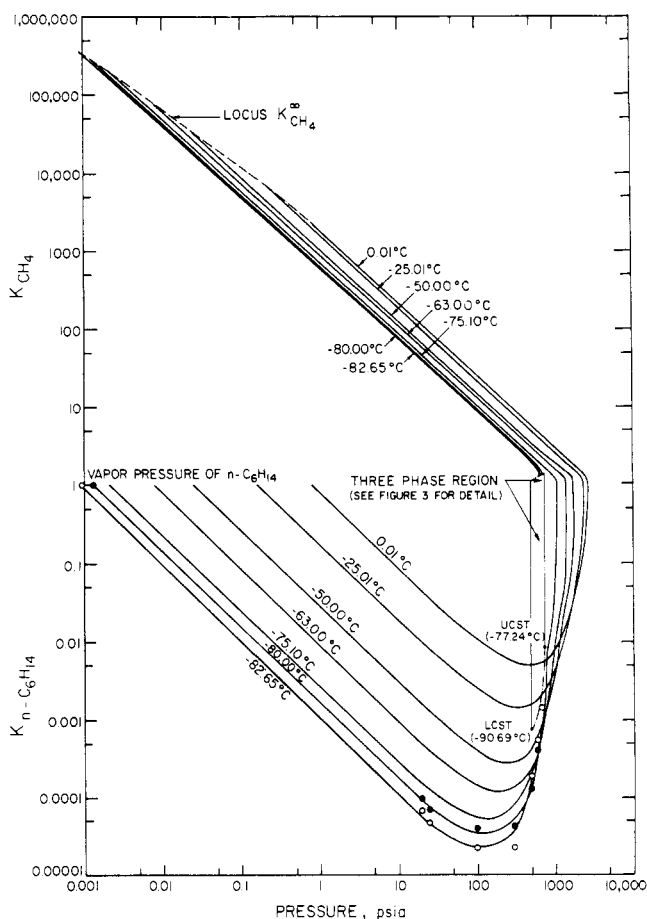


Figure 2. K value vs. pressure along isotherms for the methane-n-hexane system.

shown in Figure 2. Comparisons with BWRS equation predictions are good in general (10). Larger deviations occur at lower temperatures and pressures near critical.

Figure 3 reveals the details of the equilibrium constants between the UCST and LCST. K values and κ values are put together for each isotherm as a function of pressure in an expanded scale. The dot-dash lines are the respective loci for the

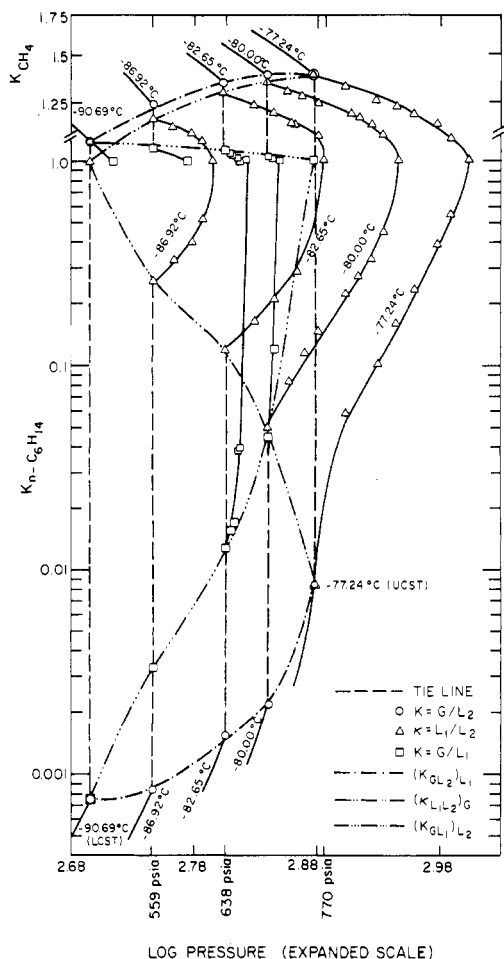


Figure 3. Equilibrium constants in the two liquid phase region.

equilibrium constants at the three phase conditions. These correspond to the dot-dash lines on Figure 1.

Cross plots of isobaric concentration vs. reciprocal absolute temperature are shown in Figure 4. Shim and Kohn's data (11) are also shown for comparison.

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Glossary

- K ratio of vapor concentration to liquid concentration
- κ ratio of light liquid concentration to heavy liquid concentration
- x liquid concentration, mole fraction
- y vapor concentration, mole fraction
- ∞ superscript denoting limiting value for the subscripted component at the limiting other pure component vapor pressure

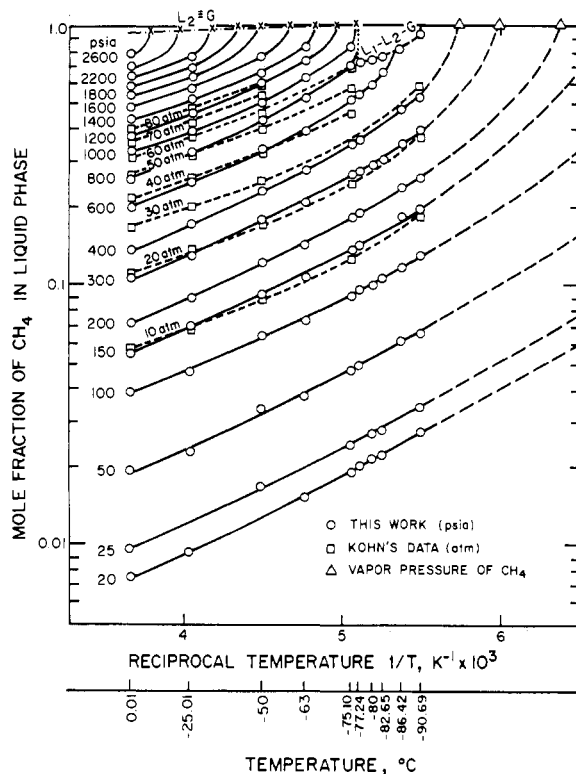


Figure 4. Isobaric bubble point behavior for the methane-*n*-hexane system.

- L_1 light liquid in equilibrium with vapor
- L_1' light liquid in equilibrium with heavy liquid
- L_2 heavy liquid in equilibrium with vapor or L_1'
- G gas phase in equilibrium with liquid
- τ temperature in three-phase region
- Π pressure in L_1 - L_2 or L_1 - G regions

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